

# Alpha Power One-Parameter Weibull Distribution: Its Properties, Simulations and Applications to Real-Life Data

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**Abstract** In this paper, we introduce a new lifetime distribution called alpha power one-parameter Weibull (APOPW) distribution based on the alpha power transformation method has been defined and studied. Various statistical properties of the newly proposed distribution including moments, moment generating function, quantile function, Rényi and Shannon entropy, stress-strength reliability, mean deviations, and extreme order statistics have been obtained. Several estimation techniques are studied, including maximum likelihood estimation (MLE), Anderson–Darling (AD), least squares estimation (LSE), Cramér–von Mises (CVM), and maximum product of spacings (MPS). The estimators compared their efficiency based on average absolute bias (BIAS), mean squared error (MSE), and mean absolute relative error (MRE), identifying that MLE as the most robust method across various sample sizes increase. The efficiency and flexibility of the new distribution are illustrated by analysing two real-live data sets, and compare its goodness-of-fit against several existing lifetime distributions.

**Keywords** Alpha power transformation, One-parameter Weibull distribution, Moment, Quantile, Estimation Methods, Simulation.

**AMS 2010 subject classifications** 60E05, 62E10.

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## 1. Introduction

In 2017, Mahdavi and Kundu [1] introduced a new method, called alpha power transformation (APT) to incorporate skewness to the baseline continuous distribution. The cumulative distribution function (CDF) for the APT family of distributions is defined as follows:

$$F_{APT}(t) = \begin{cases} \frac{\alpha^{F(t)} - 1}{\alpha - 1} & \text{if } \alpha > 0, \alpha \neq 1 \\ F(t) & \text{if } \alpha = 1 \end{cases} \quad (1)$$

The corresponding probability density function (PDF) for the APT family is given by:

$$f_{APT}(t) = \begin{cases} \frac{\log \alpha}{\alpha - 1} \alpha^{F(t)} f(t) & \text{if } \alpha > 0, \alpha \neq 1 \\ f(t) & \text{if } \alpha = 1 \end{cases} \quad (2)$$

The Weibull distribution (see Weibull 1951)[17] is a continuous probability distribution used widely in statistics and engineering. It is commonly used for analyzing biostatistics, medical, actuarial science and hydrological data sets, as one of the most popular distributions in analysing the lifetime data due to the wide variety of shapes it

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can be assumed by varying its shape parameter. The cumulative distribution function of the Weibull distribution is defined as:

$$F_W(t) = 1 - e^{-\beta t^\lambda}, \quad t, \lambda, \beta > 0. \quad (3)$$

Where  $\lambda > 0$  is the shape parameter and  $\beta > 0$  is the scale parameter.

In this paper we set  $\beta$  equal to 1 and thus the equation (3) becomes as follows:

$$F(t) = 1 - e^{-t^\lambda}, \quad t, \lambda > 0. \quad (4)$$

called the cumulative distribution function (CDF) of the One-Parameter Weibull distribution.

In this work, we introduce a new distribution called the **Alpha Power One-Parameter Weibull (APOPW)** distribution, which is derived based on the novel technique for creating new distributions, that of alpha power transformation (APT) introduced by Mahdavi and Kundu in [1]. The APOPW distribution is an extension of the classical Weibull distribution, adding a parameter for increased flexibility in modeling different hazard shapes, particularly non-monotonic ones, which the classic Weibull distribution cannot. Explore its fundamental properties. Particular attention is given to the cumulative distribution function (CDF), as well as the monotonic behavior of the probability density (PDF), Survival and hazard functions. Its statistical properties such as moments, mean, variance, moment generating function, skewness and kurtosis, quantile function, Rényi and Shannon entropy, stress-strength reliability, mean deviations, and extreme order statistics are discussed. Estimation of its parameters is made using five methods : maximum likelihood estimation (MLE), Anderson–Darling (AD), least squares estimation (LSE), Cramér–von Mises (CVM), and maximum product of spacings (MPS). Comprehensive Simulations of the model are conducted, and its applications to tow real data sets are also presented.

More recent, many generalizations of the alpha power transformation methods on modeling Weibull distributions have been attempted by various researchers, the alpha power Weibull distribution by Nassar et al. (2017) [18], a new extension of Weibull distribution called alpha power transformed Weibull distribution by Dey et al. (2017) [19], a new modified alpha power Weibull distribution by Seema et al. (2021) [30], and alpha power transformed generalized Weibull distribution by Merga et al. (2024) [21].

The paper is organized into several sections. It begins with an introduction in Section 1, introduces the new distribution by a presentation of the APOPW Model using the APT method in Section 2. Section 3 covers the derivation of survival and hazard functions for the new distribution, deriving and discussing its statistical properties. Section 4 elaborates on the several parameter estimation Methods. The later section include the presentation of a comprehensive simulation study in Section 5, an application around to model comparison in fitting to real data Sets in Section 6, and the conclusion in Section 7.

## 2. The APOPW Model

In this paper, we introduce the new distributions, called the Alpha-Power One-Parameter Weibull distribution (APOPWD for short). The probability function of APOPW with two parameters  $\alpha, \lambda$ , where  $\alpha > 0$  and  $\lambda > 0$  are the shape parameters, are obtained by using the CDF and PDF of one-parameter Weibull distribution in  $\alpha$  - power transformation. The corresponding density of the APOPW distribution of  $t > 0$  is:

$$f_{APOPW}(t) = \begin{cases} \frac{\log \alpha}{\alpha - 1} \alpha^{1 - e^{-t^\lambda}} \lambda t^{\lambda - 1} e^{-t^\lambda} & \text{if } \alpha > 0, \alpha \neq 1 \\ \lambda t^{\lambda - 1} e^{-t^\lambda} & \text{if } \alpha = 1 \end{cases} \quad (5)$$

Figure 2 shows the behavior of the density function under various parameter configurations. The results indicate that the PDF is unimodal. And the cumulative distribution function is given by :

$$F_{APOPW}(t) = \begin{cases} \frac{\alpha^{1 - e^{-t^\lambda}} - 1}{\alpha - 1} & \text{if } \alpha > 0, \alpha \neq 1 \\ 1 - e^{-t^\lambda} & \text{if } \alpha = 1 \end{cases} \quad (6)$$

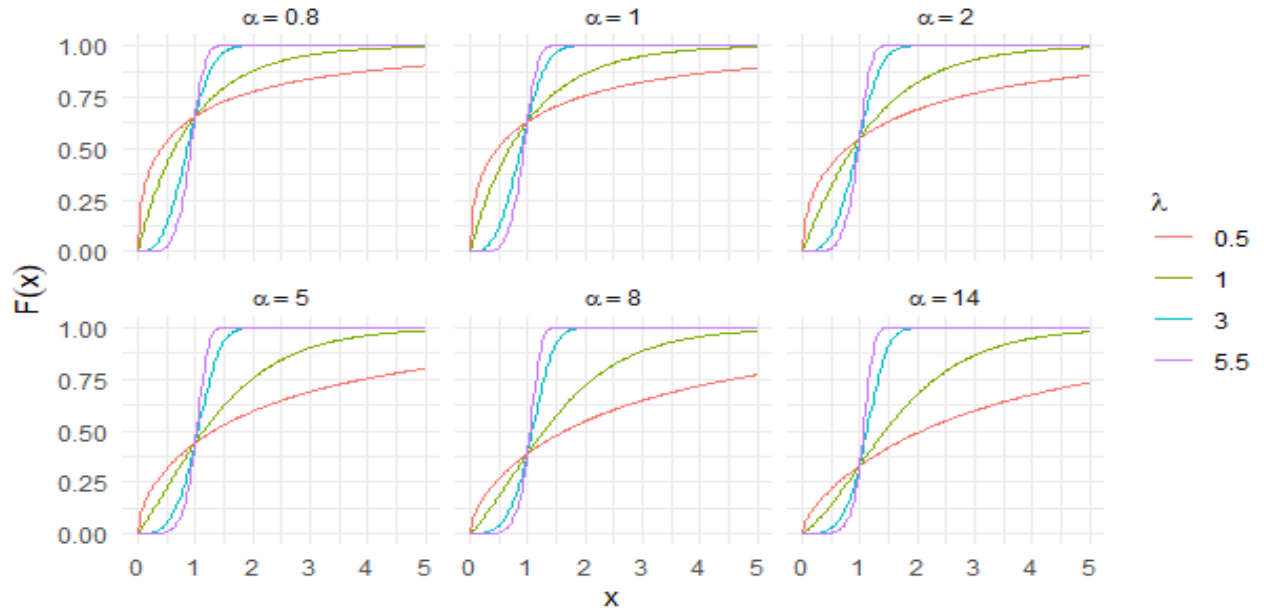


Figure 1. CDF  $F_{APOPW}(x)$  for different  $\alpha$  and  $\lambda$  values

As observed in Figure 1, the CDF increases to one at different rates depending on the parameter values.

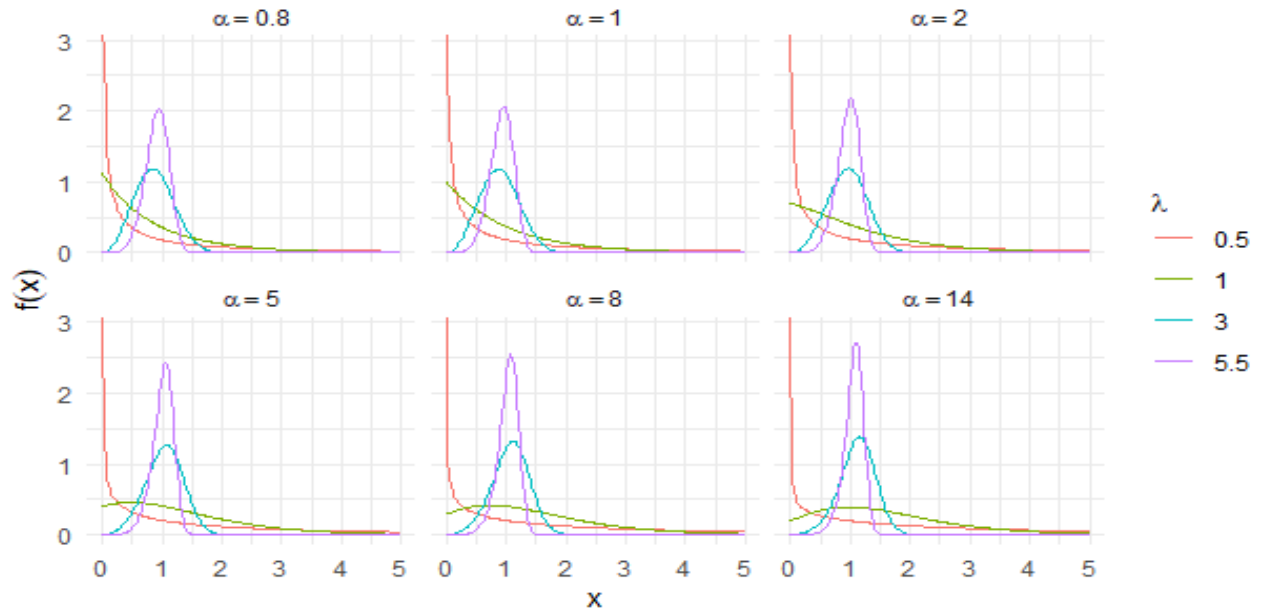


Figure 2. PDF  $f_{APOPW}(x)$  for different  $\alpha$  and  $\lambda$  values

Figure 2 Shows that for a fixed  $\lambda$ , increasing  $\alpha$  shifts the mode of the PDF to the right and elongates the tail.

## 2.1. Shape behavior

The effect of  $\lambda$ :

- Controls the spread and tail behavior of the distribution.
- Appears in the exponent and power terms:  $t^\lambda, t^{\lambda-1}$ .
- $\lambda < 1$ : Heavy right tail, high density near zero.
- $\lambda = 1$ : Exponential-like decay.
- $\lambda > 1$ : Peak shifts right, tail becomes thinner.

The effect of  $\alpha$ :

- Modulates the skewness and modality of the distribution.
- Appears in the transformation  $\alpha^{1-e^{-t^\lambda}}$ .
- $\alpha < 1$ : CDF grows slowly, PDF is flatter—more weight in the tail.
- $\alpha > 1$ : CDF grows quickly, PDF is sharper—more weight near the mode.
- $\alpha = 1$ : Distribution simplifies to the Weibull distribution.

The interactive effects of  $\alpha$  and  $\lambda$ :

The interaction between  $\alpha$  and  $\lambda$  creates nonlinear distortions in the shape of the distribution:

| $\alpha$     | $\lambda$     | PDF Behavior                | CDF Behavior             |
|--------------|---------------|-----------------------------|--------------------------|
| $\alpha < 1$ | $\lambda < 1$ | Flat, heavy-tailed          | Slow accumulation        |
| $\alpha > 1$ | $\lambda < 1$ | Sharp near zero, fast decay | Rapid accumulation early |
| $\alpha < 1$ | $\lambda > 1$ | Broad peak, long tail       | Gradual rise             |
| $\alpha > 1$ | $\lambda > 1$ | Narrow peak, short tail     | Steep rise then plateau  |

So,

- $\lambda$  shapes the core decay and spread—it's the engine of the Weibull-like behavior.
- $\alpha$  acts as a distortion lens, warping the distribution to be more peaked or more spread out.
- When  $\alpha = 1$ , the distortion disappears and the distribution becomes Weibull.
- Together,  $\alpha$  and  $\lambda$  allow the APOPW distribution to flexibly model a wide range of behaviors—from early failures to long lifetimes, from sharp peaks to heavy tails.

### Theorem 1

The function of the new formula for the APOPW distribution is a PDF.

#### Proof

The function of the new formula for the APOPW distribution to be a PDF if  $f_{APOPW}(t) > 0$  and  $\int_0^\infty f_{APOPW}(t) dt = 1$ . Then

$$\int_0^\infty f_{APOPW}(t) dt = \int_0^\infty \frac{\log \alpha}{\alpha - 1} \alpha^{1-e^{-t^\lambda}} \lambda t^{\lambda-1} e^{-t^\lambda} dt \quad (7)$$

Let use  $\delta = 1 - e^{-t^\lambda}$ , then the derivatives give  $\frac{d\delta}{dt} = \lambda t^{\lambda-1} e^{-t^\lambda}$  and  $dt = \frac{d\delta}{\lambda t^{\lambda-1} e^{-t^\lambda}}$ , so

$$\int_0^\infty f_{APOPW}(t) dt = \frac{\log \alpha}{\alpha - 1} \int_0^\infty \frac{\alpha^{1-e^{-t^\lambda}} \lambda t^{\lambda-1} e^{-t^\lambda}}{\lambda t^{\lambda-1} e^{-t^\lambda}} d\delta = \frac{\log \alpha}{\alpha - 1} \int_0^\infty \alpha^\delta d\delta \quad (8)$$

using exponential rule  $\int \alpha^\delta d\delta = \frac{\alpha^\delta}{\log \alpha}$ , then

$$\int_0^{\infty} f_{APOPW}(t) dt = \frac{\log \alpha}{\alpha - 1} \int_0^{\infty} \alpha^{\delta} d\delta = \frac{\log \alpha}{\alpha - 1} \frac{\alpha^{\delta}}{\log \alpha} \Big|_0^{\infty} = \frac{\alpha^{1-e^{-t^{\lambda}}}}{\alpha - 1} \Big|_0^{\infty} = 1 \quad (9)$$

Hence, it indicates that  $f_{APOPW}(t)$  satisfies the definition of PDF.

### 3. Main properties

#### 3.1. Survival and hazard functions

The survival functions corresponding to the CDF defined in (6) are given by

$$S_{APOPW}(t) = \begin{cases} \frac{\alpha}{\alpha-1} (1 - \alpha^{-e^{-t^{\lambda}}}) & \text{if } \alpha > 0, \alpha \neq 1 \\ e^{-t^{\lambda}} & \text{if } \alpha = 1 \end{cases} \quad (10)$$

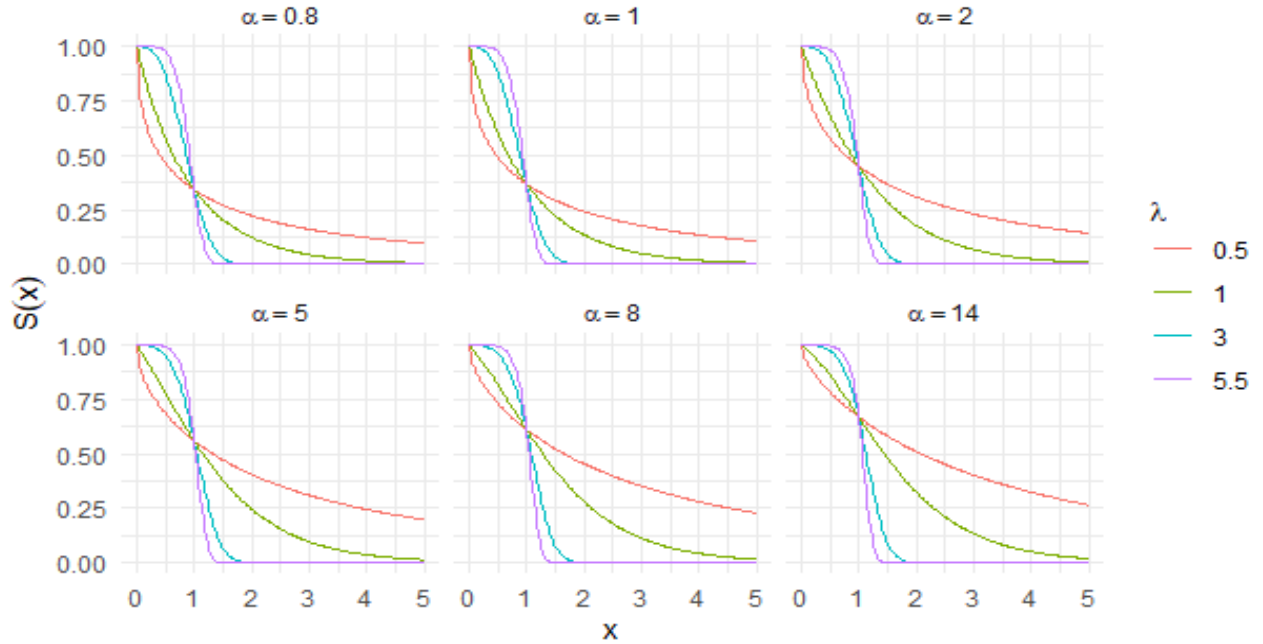


Figure 3. Survival curves for APOPWD for different  $\alpha$  and  $\lambda$  values

Figure 3 Shows that for a fixed  $\lambda$ , increasing  $\alpha$  shifts the mode of the survival function to the right and elongates the tail.

and the hazard functions are given by

$$h_{APOPW}(t) = \begin{cases} \frac{\log(\alpha) \lambda t^{\lambda-1} e^{-t^{\lambda}}}{\alpha^{e^{-t^{\lambda}}} - 1} & \text{if } \alpha > 0, \alpha \neq 1 \\ \lambda t^{\lambda-1} & \text{if } \alpha = 1 \end{cases} \quad (11)$$

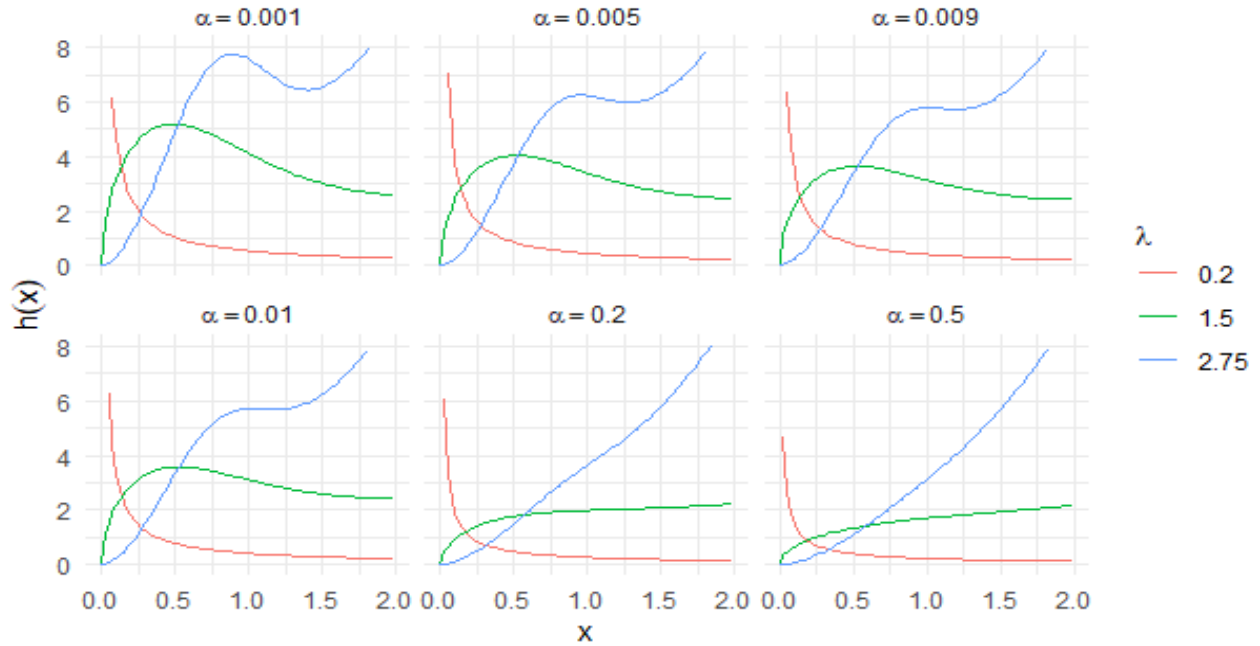


Figure 4. Hazard function  $h_{APOPW}(t)$  for different  $\alpha$  and  $\lambda$  values.

The hazard function exhibits diverse shapes depending on the parameters  $\alpha$  and  $\lambda$ . For  $\alpha < 1$ , the hazard rate is typically decreasing, indicating early failures. For  $\alpha > 1$ , it becomes increasing, suggesting aging or wear-out mechanisms. In some cases, particularly when  $\alpha$  is very small and  $\lambda$  is moderate, the hazard function may exhibit a *bathtub shape*, which is common in reliability studies. This flexibility makes the distribution suitable for modeling various lifetime behaviors.

### 3.2. The Moments and Moment Generating Function

The  $k$ th Moments for the APOPWD distribution are defined as follows:

$$\begin{aligned} E(T^x) &= \int_0^\infty t^x f_{APOPW}(t) dt \\ &= \int_0^\infty t^x \frac{\log \alpha}{\alpha - 1} \alpha^{1-e^{-t^\lambda}} \lambda t^{\lambda-1} e^{-t^\lambda} dt \end{aligned}$$

using the following string representation:

$$\alpha^{-z} = \sum_{k=0}^{\infty} \frac{(-\log \alpha)^k z^k}{k!} \quad (12)$$

expanding  $\alpha^{-e^{-t^\lambda}}$  in PDF and letting  $z = e^{-t^\lambda}$ , then the density of APOPW distribution can be written as follows:

$$f_{APOPW}(t) = \frac{\alpha \log \alpha}{\alpha - 1} \lambda t^{\lambda-1} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^k}{k!} \left(e^{-t^\lambda}\right)^k e^{-t^\lambda} = \frac{\alpha}{1 - \alpha} \lambda t^{\lambda-1} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} e^{-(k+1)t^\lambda} \quad (13)$$

Now, we can obtain the moments :

$$\begin{aligned} E(T^x) &= \int_0^\infty t^x \frac{\alpha}{1-\alpha} \lambda t^{\lambda-1} \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k!} e^{-(k+1)t^\lambda} dt \\ &= \frac{\alpha}{1-\alpha} \lambda \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k!} \int_0^\infty t^{x+\lambda-1} e^{-(k+1)t^\lambda} dt \end{aligned} \quad (14)$$

Let use  $u = (k+1)t^\lambda$ , then the derivatives of  $z$  with respect to  $t$  give  $\frac{du}{dt} = (k+1)\lambda t^{\lambda-1}$ , so

$$\begin{aligned} E(T^x) &= \frac{\alpha}{1-\alpha} \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)} \int_0^\infty \left( \left( \frac{u}{(k+1)} \right)^{\frac{1}{\lambda}} \right)^x e^{-u} du \\ &= \frac{\alpha}{1-\alpha} \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1) (k+1)^{\frac{x}{\lambda}}} \int_0^\infty u^{\frac{x}{\lambda}} e^{-u} du \\ E(T^x) &= \frac{\alpha}{1-\alpha} \Gamma\left(\frac{x}{\lambda} + 1\right) \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{x}{\lambda}+1}} \end{aligned} \quad (15)$$

The moment generating function  $M_T(x)$  of the APOPW distribution For a continuous random variable  $T$ , is given by

$$M_T(\nu) = E(e^{\nu T}) = \int_0^\infty e^{\nu t} f_{APOPW}(t) dt \quad (16)$$

Using series representation  $e^{\nu t} = \sum_{x=0}^\infty \frac{(\nu t)^x}{x!}$ , so

$$\begin{aligned} M_T(\nu) &= \int_0^\infty \sum_{x=0}^\infty \frac{(\nu t)^x}{x!} f_{APOPW}(t) dt = \sum_{x=0}^\infty \frac{(\nu)^x}{x!} \int_0^\infty t^x f_{APOPW}(t) dt = \sum_{x=0}^\infty \frac{(\nu)^x}{x!} E(T^x) \\ &= \frac{\alpha}{1-\alpha} \sum_{k=0}^\infty \sum_{x=0}^\infty \frac{(-\log \alpha)^{k+1} (\nu)^x \Gamma\left(\frac{x}{\lambda} + 1\right)}{x! k! (k+1)^{\frac{x}{\lambda}+1}} \end{aligned} \quad (17)$$

The mean

$$\mu = E(T) = \frac{\alpha}{1-\alpha} \Gamma\left(\frac{1}{\lambda} + 1\right) \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{1}{\lambda}+1}} \quad (18)$$

The variance of the APOPW distribution is

$$Var(T) = \frac{\alpha}{1-\alpha} \Gamma\left(\frac{2}{\lambda} + 1\right) \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{2}{\lambda}+1}} - \left( \frac{\alpha}{1-\alpha} \Gamma\left(\frac{1}{\lambda} + 1\right) \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{1}{\lambda}+1}} \right)^2 \quad (19)$$

We obtained now the coefficient of variation  $\lambda$ , skewness and kurtosis of the APOPW distribution

$$C.V = \frac{\sqrt{\frac{\alpha}{1-\alpha} \Gamma\left(\frac{2}{\lambda} + 1\right) \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{2}{\lambda}+1}} - \left( \frac{\alpha}{1-\alpha} \Gamma\left(\frac{1}{\lambda} + 1\right) \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{1}{\lambda}+1}} \right)^2}}{\frac{\alpha}{1-\alpha} \Gamma\left(\frac{1}{\lambda} + 1\right) \sum_{k=0}^\infty \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{1}{\lambda}+1}}}$$

$$\begin{aligned}
skewness &= \frac{\frac{\alpha}{1-\alpha} \Gamma(\frac{3}{\lambda} + 1) \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!(k+1)^{\frac{3}{\lambda}+1}}}{\left\{ \frac{\alpha}{1-\alpha} \Gamma(\frac{2}{\lambda} + 1) \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!(k+1)^{\frac{2}{\lambda}+1}} - \left( \frac{\alpha}{1-\alpha} \Gamma(\frac{1}{\lambda} + 1) \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!(k+1)^{\frac{1}{\lambda}+1}} \right)^2 \right\}^{\frac{3}{2}}} \\
kurtosis &= \frac{\frac{\alpha}{1-\alpha} \Gamma(\frac{4}{\lambda} + 1) \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!(k+1)^{\frac{4}{\lambda}+1}}}{\left\{ \frac{\alpha}{1-\alpha} \Gamma(\frac{2}{\lambda} + 1) \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!(k+1)^{\frac{2}{\lambda}+1}} - \left( \frac{\alpha}{1-\alpha} \Gamma(\frac{1}{\lambda} + 1) \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!(k+1)^{\frac{1}{\lambda}+1}} \right)^2 \right\}^2}
\end{aligned}$$

### 3.3. Quantile function

The quantile function  $T$  of the APOPW distribution is given by

$$t_{\beta} = \left\{ -\log \left( \frac{\log(\alpha / ((\alpha - 1)\beta + 1))}{\log \alpha} \right) \right\}^{\frac{1}{\lambda}} \quad (20)$$

where  $F_{APOPW}(t) = \beta = \frac{\alpha^{1-e^{-t^{\lambda}}}-1}{\alpha-1}$  and then  $t = F_{APOPW}^{-1}(\beta)$ . For more details see [2].  
The median of the APOPW distribution can be obtained as

$$M = t_{\frac{1}{2}} = \left\{ -\log \left( \frac{\log(2\alpha / (\alpha + 1))}{\log \alpha} \right) \right\}^{\frac{1}{\lambda}} \quad (21)$$

### 3.4. The Rényi and Shannon Entropy

The entropy of a random variable  $T$  is a measure of variation of uncertainty (see, Rényi, 1961) [3], that of the Alpha Power one-parameter distribution is given by

$$I_{RE}(s) = \frac{1}{1-s} \log \left( \int_{-\infty}^{+\infty} f_{APOPW}(t)^s dt \right) \quad (22)$$

where  $s$  (integer)  $> 0$  and  $s \neq 0$ . Using the PDF in (13) we have:

$$\begin{aligned}
I_{RE}(s) &= \frac{1}{1-s} \log \left( \int_0^{+\infty} \left\{ \frac{\alpha}{1-\alpha} \lambda t^{\lambda-1} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} e^{-(k+1)t^{\lambda}} \right\}^s dt \right) \\
&= \frac{1}{1-s} \log \left( \left\{ \frac{\alpha}{1-\alpha} \lambda \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} \right\}^s \int_0^{+\infty} t^{s(\lambda-1)} e^{-s(k+1)t^{\lambda}} dt \right)
\end{aligned} \quad (23)$$

Let  $v = s(k+1)t^{\lambda} \Rightarrow \frac{dv}{dt} = \lambda s(k+1)t^{\lambda-1}$ , the Rényi entropy reduces to

$$\begin{aligned}
I_{RE}(s) &= \frac{1}{1-s} \log \left( \left\{ \frac{\alpha}{1-\alpha} \lambda \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} \right\}^s \int_0^{+\infty} \left( \frac{v}{s(k+1)} \right)^{\frac{(\lambda-1)(s-1)}{\lambda}} \frac{e^{-v}}{\lambda s(k+1)} dv \right) \\
&= \frac{s}{1-s} \log \left\{ \frac{\alpha}{1-\alpha} \lambda \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} \right\} + \frac{1}{1-s} \log \left\{ \frac{\Gamma \left( \frac{(\lambda-1)(s-1)}{\lambda} + 1 \right)}{\lambda \{s(k+1)\}^{\frac{(\lambda-1)(s-1)}{\lambda} + 1}} \right\}
\end{aligned} \quad (24)$$



The Shannon entropy  $SE_T$  from a random variable  $T$  is defined as

$$SE_T = - \int_{-\infty}^{+\infty} f_{APOPW}(t) \log f_{APOPW}(t) dt \quad (25)$$

Using the PDF in (13),  $SE_T$  is

$$SE_T = \log \left( \frac{\alpha - 1}{\alpha \lambda \log \alpha} \right) + \frac{\alpha}{\alpha - 1} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} \left( \frac{\log \alpha}{k+2} - \frac{1}{(k+1)^2} + (\lambda - 1) \lambda I \right) \quad (26)$$

where

$$I = \int_0^{\infty} t^{\lambda-1} e^{-(k+1)t^{\lambda}} \log t dt$$

Now by applying the transformation  $t^{\lambda} = y$  and

$$\int_0^{\infty} e^{-\vartheta t} \log t dt = -\frac{1}{\vartheta} (c + \log \vartheta)$$

where  $c$  is the Euler constant. Then the Shannon entropy  $SE_T$  is derived as :

$$SE_T = \log \left( \frac{\alpha - 1}{\alpha \lambda \log \alpha} \right) + \frac{\alpha}{\alpha - 1} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} \left( \frac{\log \alpha}{k+2} - \frac{1}{(k+1)^2} + \frac{(1 - \lambda) (c + \log (k+1))}{(k+1) \lambda} \right) \quad (27)$$

### 3.5. Stress-Strength Reliability

The measure of reliability has many applications, especially in the area of engineering. The component fails at the instant that the random stress  $T_2$  applied to it exceeds the random strength  $T_1$ , and the component will function satisfactorily whenever  $T_1 > T_2$ . Hence,  $R = P[T_2 < T_1]$  is a measure of component reliability. We derive the reliability  $R$  when  $T_1$  and  $T_2$  have independent  $APOPW(\alpha_1, \lambda)$  and  $APOPW(\alpha_2, \lambda)$  distributions. The reliability is defined by

$$\begin{aligned} R &= P[T_2 < T_1] = \int_0^{\infty} f_1(t; \alpha_1, \lambda) F_2(t; \alpha_2, \lambda) dt \\ &= \int_0^{\infty} \frac{\log \alpha_1}{\alpha_1 - 1} \alpha_1^{1-e^{-t^{\lambda}}} \lambda t^{\lambda-1} e^{-t^{\lambda}} \left( \frac{\alpha_2^{1-e^{-t^{\lambda}}} - 1}{\alpha_2 - 1} \right) dt \end{aligned} \quad (28)$$

Using the string representation in equation (12),  $R$  can be written as :

$$R = \frac{\lambda \alpha_1 \alpha_2 \log \alpha_1}{(\alpha_1 - 1)(\alpha_2 - 1)} \sum_{k=0}^{\infty} \sum_{m=0}^{\infty} \frac{(-\log \alpha_1)^k (-\log \alpha_2)^m}{k! m!} \int_0^{\infty} t^{\lambda-1} e^{-(k+m+1)t^{\lambda}} dt - \frac{1}{\alpha_2 - 1} \quad (29)$$

By using the transformation  $y = (k + m + 1) t^{\lambda}$ , the stress-strength reliability reduces to

$$\begin{aligned}
R &= \frac{\lambda \alpha_1 \alpha_2 \log \alpha_1}{(\alpha_1 - 1)(\alpha_2 - 1)} \sum_{k=0}^{\infty} \sum_{m=0}^{\infty} \frac{(-\log \alpha_1)^k (-\log \alpha_2)^m}{k!m!} \int_0^{+\infty} \left( \frac{y}{(k+m+1)} \right)^{\frac{\lambda-1}{\lambda}} \\
&\quad \times \frac{e^{-y}}{\lambda (k+m+1) \left( \frac{y}{(k+m+1)\beta} \right)^{\frac{\lambda-1}{\lambda}}} dy - \frac{1}{\alpha_2 - 1} \\
R &= \frac{1}{\alpha_2 - 1} \left( \frac{\alpha_1 \alpha_2}{(1 - \alpha_1)} \sum_{k=0}^{\infty} \sum_{m=0}^{\infty} \frac{(-\log \alpha_1)^{k+1} (-\log \alpha_2)^m}{k!m! (k+m+1)} - 1 \right)
\end{aligned} \tag{30}$$

### 3.6. Mean deviations

The deviation from the mean and the median are used to measure the dispersion and spread in a population from the centre. The mean deviation from the mean and median can be written as

$$D(\mu) = \int_0^{\infty} |t - \mu| f_{APOPW}(t) dt = 2\mu F_{APOPW}(\mu) - 2 \int_0^{\mu} t f_{APOPW}(t) dt, \tag{31}$$

$$D(M) = \int_0^{\infty} |t - M| f_{APOPW}(t) dt = \mu - 2 \int_0^M t f_{APOPW}(t) dt. \tag{32}$$

where  $D(\mu)$  and  $D(M)$  is the mean deviation from the mean and median respectively.

Using the PDF in (13) and the transformation  $u = (k+1)t^\lambda$ , the required integral becomes :

$$\begin{aligned}
\int_0^b t f_{APOP}(t) dt &= \frac{\alpha}{1-\alpha} \lambda \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k!} \int_0^b t^\lambda e^{-(k+1)t^\lambda} dt \\
&= \frac{\alpha}{1-\alpha} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{1}{\lambda}+1}} \gamma \left( \frac{1}{\lambda} + 1, (k+1)b^\lambda \right)
\end{aligned}$$

where  $\gamma$  is the lower incomplete gamma function.

we obtain,

$$\begin{aligned}
D(\mu) &= 2\mu F_{APOPW}(\mu) - 2 \int_0^{\mu} t f_{APOPW}(t) dt, \\
&= 2\mu F_{APOPW}(\mu) - \frac{\alpha}{1-\alpha} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{1}{\lambda}+1}} \gamma \left( \frac{1}{\lambda} + 1, (k+1)\mu^\lambda \right).
\end{aligned} \tag{33}$$

and

$$\begin{aligned}
D(M) &= \mu - 2 \int_0^M t f_{APOPW}(t) dt, \\
&= \mu - \frac{\alpha}{1-\alpha} \sum_{k=0}^{\infty} \frac{(-\log \alpha)^{k+1}}{k! (k+1)^{\frac{1}{\lambda}+1}} \gamma \left( \frac{1}{\lambda} + 1, (k+1)M^\lambda \right).
\end{aligned} \tag{34}$$

### 3.7. Extreme order statistics of APOPW

Let  $T_1, T_2, \dots, T_n$  be a sample of  $n$  random variables that follows the APOPW distribution. For  $\alpha = 1$ , the APOPW reduces to one-parameter Weibull distribution. The asymptotic distribution of the sample maximum is of extreme type. According to Arnold et al. (2008) [22], we find that the asymptotic distribution of the sample minimum of  $T_{1,n}$  is Weibull type with shape parameter  $\lambda > 0$ :

$$\lim_{x \rightarrow 0} \frac{F_{APOPW}(xt)}{F_{APOPW}(x)} = t$$

and

$$\lim_{x \rightarrow \infty} \frac{f_{APOPW}(xt)}{f_{APOPW}(x)} = t^{\lambda-1}.$$

## 4. Estimation Methods

### Maximum likelihood estimation

Let  $T_1, T_2, \dots, T_n$  be a random sample of size  $n$  taken from the APOPW distribution. Then the log-likelihood function is given by

$$\begin{aligned} \ln L(\alpha, \lambda) &= \ln \left\{ \prod_{i=1}^n f_{APOP}(t_i; \alpha, \lambda) \right\} \\ &= \ln \left\{ \prod_{i=1}^n \frac{\log}{\alpha - 1} \alpha^{1-e^{-t_i^\lambda}} \lambda t_i^{\lambda-1} e^{-t_i^\lambda} \right\} \\ &= \ln \left\{ \left( \frac{\lambda \alpha \log \alpha}{\alpha - 1} \right)^n \prod_{i=1}^n \alpha^{-e^{-t_i^\lambda}} t_i^{\lambda-1} e^{-t_i^\lambda} \right\} \\ &= n \ln \left( \frac{\log \alpha}{\alpha - 1} \right) + n \ln \lambda \alpha + (\lambda - 1) \sum_{i=1}^n \ln t_i - \ln \alpha \sum_{i=1}^n e^{-t_i^\lambda} - \sum_{i=1}^n t_i^\lambda \end{aligned} \quad (35)$$

Determining the maximum likelihood estimators for the parameters  $\alpha$  and  $\lambda$  requires the use of numerical methods, such as the Newton-Raphson or BFGS algorithms, because the likelihood function is nonlinear.

### Least Squares Estimators

Gauss is credited with developing the least squares approach, which is a kind of estimation. It is typically applied to the linear model's parameter estimate. Swain, Venkatraman, and Wilson (1988) [16] estimated the parameters of beta distributions using least squares estimates and weighted least squares estimates. Also see Alkawasbeh and Raqab (2009) [4], Gupta and Kundu (2001) [8], and Kundu and Raqab (2005) [9].

Let  $T_1, T_2, \dots, T_n$  be order statistics from a random sample of size  $n$  from a distribution function  $F(\cdot)$  and suppose  $T_{(i)}$  denotes the ordered sample. The proposed method uses the distribution of  $F(T_{(i)})$ ,  $i = 1, 2, \dots, n$ . For a sample of size  $n$ , we have:

$$\begin{aligned} \mathbb{E}[F(T_{(i)})] &= \frac{i}{n+1}, \quad \text{Var}[F(T_{(i)})] = \frac{i(n-i+1)}{(n+1)^2(n+2)}, \\ \text{Cov}(F(T_{(i)}), F(T_{(j)})) &= \frac{i(n-j+1)}{(n+1)^2(n+2)}, \quad \text{for } i < j. \end{aligned}$$

The least squares estimates can be obtained by minimizing:

$$\sum_{i=1}^n \left( F(T_{(i)}) - \frac{i}{n+1} \right)^2$$

with respect to the unknown parameters.

### ***Methods of Anderson-Darling***

In 1952, Anderson and Darling [12] created the Anderson-Darling test to identify sample distributions that deviate from normal. This test served as an alternative to existing statistical tests in this regard. According to Anderson and Darling (1954) [13], Pettitt (1976) [7], and Stephens (2013) [14], the AD test specifically converges very rapidly towards the asymptote.

The Anderson-Darling estimators of parameters are obtained by minimizing the function:

$$AD = -n - \frac{1}{n} \sum_{i=1}^n (2i-1) [\log(F(t_{(i)})) + \log(S(t_{(i)}))]$$

### ***The Cramér-von Mises Estimation***

Macdonald (1971) [10] provides empirical support for the selection of Cramér-von Mises type minimum distance estimators, demonstrating that the estimator's bias is lower than that of other minimum distance estimators.

The Cramér-von Mises estimate of the parameters is obtained by minimizing:

$$C = \frac{1}{12n} \sum_{i=1}^n \left( F(t_{(i)}) - \frac{2i-1}{2n} \right)^2$$

### ***Method of Maximum Product of Spacings***

The maximum product of spacings (MPS) approach was presented by Cheng and Amin (1979 [5], 1983 [6]) as a substitute for MLE in the estimation of parameters for continuous univariate distributions. A similar technique was independently developed as an estimate for the Kullback-Leibler measure of information by Ranney (1984) [11].

The estimation of parameters is carried out by maximizing the following equation:

$$X = \left( \prod_{i=1}^{n+1} D_i \right)^{1/(n+1)}, \quad \text{or, equivalently,}$$

$$\log(X) = \frac{1}{n+1} \sum_{i=1}^{n+1} \log(D_i), \quad \text{where } D_i = F(t_{(i)}) - F(t_{(i-1)})$$

## 5. Simulation

Using a simulation study, we generate samples (with increasing sample sizes) from the new APOPW distribution with given parameter values and estimate them back using the Maximum Likelihood Estimation (MLE), Anderson–Darling (AD), Cramér–von Mises (CVM), Maximum Product of Spacings (MPS), and Ordinary Least Squares (OLS) methods. To generate random samples, we employed the inverse transform sampling technique: independent uniform random numbers  $U_1, \dots, U_n \sim \text{Uniform}(0, 1)$  were generated, and each was transformed via the quantile function  $Q_F(u; \theta)$ . Since the quantile function does not admit a closed form, it was obtained numerically by solving

$$F_X(x; \theta) = u, \quad 0 < u < 1,$$

for  $x$  using a root-finding routine. This ensures that all simulated data are exact realizations from the specified distribution. The performance of the estimation methods is then measured using the mean square error (MSE), bias, and mean relative error (MRE) for each case. Different sample sizes are considered in the experiments, ranging from  $n = 25$  to 1000, and various values of the parameters  $\alpha$  and  $\lambda$  are used. These methods of estimation asymptotically converge in probability to the actual parameter values, and the solution is unique.

The results in Tables 1 to 4 and the figures from 5 to 8 show that all methods of the estimation approach the true value as the sample size increases, but the MLE is the best. The results show that as the sample size increases, the parameter estimates approach the true values, with the respective MSE, bias, and MRE computed values all approaching zero. This is also shown to be true for each case of the four simulation studies. The evaluation of estimation method efficacy in this investigation is based on the utilization of Three specific metrics, delineated as follows:

1. The average of absolute bias (BIAS):

$$|\text{bias}(\hat{\theta})| = \frac{1}{N} \sum_{i=1}^N |(\hat{\theta}_i - \theta_0)|. \quad (36)$$

2. The mean squared error (MSE):

$$\text{MSE}(\hat{\theta}) = \frac{1}{N} \sum_{i=1}^N (\hat{\theta}_i - \theta_0)^2. \quad (37)$$

3. The mean absolute relative error (MRE):

$$\text{MRE}(\hat{\theta}) = \frac{1}{N} \sum_{i=1}^N \frac{|\hat{\theta}_i - \theta_0|}{\theta_0}. \quad (38)$$

Where  $\hat{\theta} = (\hat{\alpha}, \hat{\lambda})$ .

Table 1. Simulation values of Estimates, Bias, MSE, and MRE for ( $\alpha = 0.25, \lambda = 0.75$ ).

| Sample Size | Method | $\hat{\alpha}$ | $\hat{\lambda}$ | Bias( $\hat{\alpha}$ ) | Bias( $\hat{\lambda}$ ) | MSE( $\hat{\alpha}$ ) | MSE( $\hat{\lambda}$ ) | MRE( $\hat{\alpha}$ ) | MRE( $\hat{\lambda}$ ) |
|-------------|--------|----------------|-----------------|------------------------|-------------------------|-----------------------|------------------------|-----------------------|------------------------|
| 25          | MLE    | 0.324369       | 0.813353        | 0.179711               | 0.108679                | 0.076437              | 0.019392               | 0.718845              | 0.144905               |
| 50          | MLE    | 0.271795       | 0.771895        | 0.105164               | 0.053250                | 0.026644              | 0.005048               | 0.420656              | 0.071000               |
| 100         | MLE    | 0.267370       | 0.770592        | 0.089287               | 0.048144                | 0.012593              | 0.004043               | 0.357147              | 0.064192               |
| 150         | MLE    | 0.258696       | 0.761456        | 0.072934               | 0.041724                | 0.008692              | 0.002739               | 0.291737              | 0.055632               |
| 300         | MLE    | 0.250777       | 0.758737        | 0.044352               | 0.026779                | 0.003045              | 0.001197               | 0.177407              | 0.035705               |
| 500         | MLE    | 0.257296       | 0.754542        | 0.033648               | 0.022357                | 0.001826              | 0.000732               | 0.134593              | 0.029809               |
| 1000        | MLE    | 0.249704       | 0.750975        | 0.023988               | 0.014207                | 0.000837              | 0.000306               | 0.095952              | 0.018942               |
| 25          | AD     | 0.396285       | 0.741796        | 0.231119               | 0.103433                | 0.200720              | 0.016522               | 0.924475              | 0.137910               |
| 50          | AD     | 0.303949       | 0.752035        | 0.120141               | 0.076031                | 0.026041              | 0.009526               | 0.480562              | 0.101374               |
| 100         | AD     | 0.245611       | 0.754589        | 0.073828               | 0.043996                | 0.007876              | 0.003138               | 0.295310              | 0.058662               |
| 150         | AD     | 0.255527       | 0.756381        | 0.067221               | 0.042240                | 0.007268              | 0.003011               | 0.268884              | 0.056320               |
| 300         | AD     | 0.249384       | 0.750655        | 0.046625               | 0.030872                | 0.003050              | 0.001492               | 0.186500              | 0.041162               |
| 500         | AD     | 0.254486       | 0.748928        | 0.032611               | 0.022270                | 0.001876              | 0.000806               | 0.130442              | 0.029693               |
| 1000        | AD     | 0.245710       | 0.752525        | 0.022046               | 0.017482                | 0.000744              | 0.000458               | 0.088184              | 0.023310               |
| 25          | CVM    | 0.298819       | 0.792968        | 0.191086               | 0.130043                | 0.079134              | 0.025123               | 0.764342              | 0.173391               |
| 50          | CVM    | 0.281107       | 0.768103        | 0.125054               | 0.087496                | 0.028446              | 0.014256               | 0.500216              | 0.116661               |
| 100         | CVM    | 0.264641       | 0.757663        | 0.094035               | 0.068163                | 0.016109              | 0.007417               | 0.376140              | 0.090885               |
| 150         | CVM    | 0.265220       | 0.752102        | 0.067040               | 0.047200                | 0.008889              | 0.003557               | 0.268159              | 0.062933               |
| 300         | CVM    | 0.248879       | 0.757505        | 0.042238               | 0.036216                | 0.002827              | 0.002163               | 0.168954              | 0.048288               |
| 500         | CVM    | 0.254776       | 0.753045        | 0.035079               | 0.028135                | 0.002009              | 0.001278               | 0.140315              | 0.037513               |
| 1000        | CVM    | 0.253803       | 0.751619        | 0.028523               | 0.019872                | 0.001191              | 0.000584               | 0.114093              | 0.026496               |
| 25          | MPS    | 0.359585       | 0.717946        | 0.189287               | 0.101523                | 0.107988              | 0.014917               | 0.757149              | 0.135364               |
| 50          | MPS    | 0.316639       | 0.713727        | 0.131460               | 0.076779                | 0.049231              | 0.008451               | 0.525840              | 0.102373               |
| 100         | MPS    | 0.288796       | 0.719775        | 0.086983               | 0.045951                | 0.013935              | 0.003244               | 0.347933              | 0.061269               |
| 150         | MPS    | 0.267216       | 0.728722        | 0.065284               | 0.041768                | 0.006981              | 0.002664               | 0.261134              | 0.055691               |
| 300         | MPS    | 0.261940       | 0.740038        | 0.042325               | 0.027451                | 0.003190              | 0.001164               | 0.169301              | 0.036602               |
| 500         | MPS    | 0.253688       | 0.745564        | 0.031612               | 0.021930                | 0.001729              | 0.000767               | 0.126446              | 0.029240               |
| 1000        | MPS    | 0.257929       | 0.746072        | 0.026261               | 0.015204                | 0.001116              | 0.000349               | 0.105043              | 0.020273               |
| 25          | OLS    | 0.354414       | 0.740086        | 0.201054               | 0.107783                | 0.080182              | 0.020045               | 0.804215              | 0.143711               |
| 50          | OLS    | 0.309470       | 0.731532        | 0.133111               | 0.082354                | 0.038424              | 0.009795               | 0.532443              | 0.109806               |
| 100         | OLS    | 0.262265       | 0.750616        | 0.083670               | 0.054020                | 0.011016              | 0.004548               | 0.334682              | 0.072026               |
| 150         | OLS    | 0.259752       | 0.749154        | 0.067524               | 0.050141                | 0.007154              | 0.004143               | 0.270096              | 0.066855               |
| 300         | OLS    | 0.265572       | 0.741730        | 0.045741               | 0.033617                | 0.003368              | 0.001833               | 0.182964              | 0.044823               |
| 500         | OLS    | 0.249839       | 0.745994        | 0.037211               | 0.027198                | 0.002394              | 0.001072               | 0.148843              | 0.036263               |
| 1000        | OLS    | 0.254805       | 0.750165        | 0.026729               | 0.020412                | 0.001095              | 0.000650               | 0.106914              | 0.027217               |

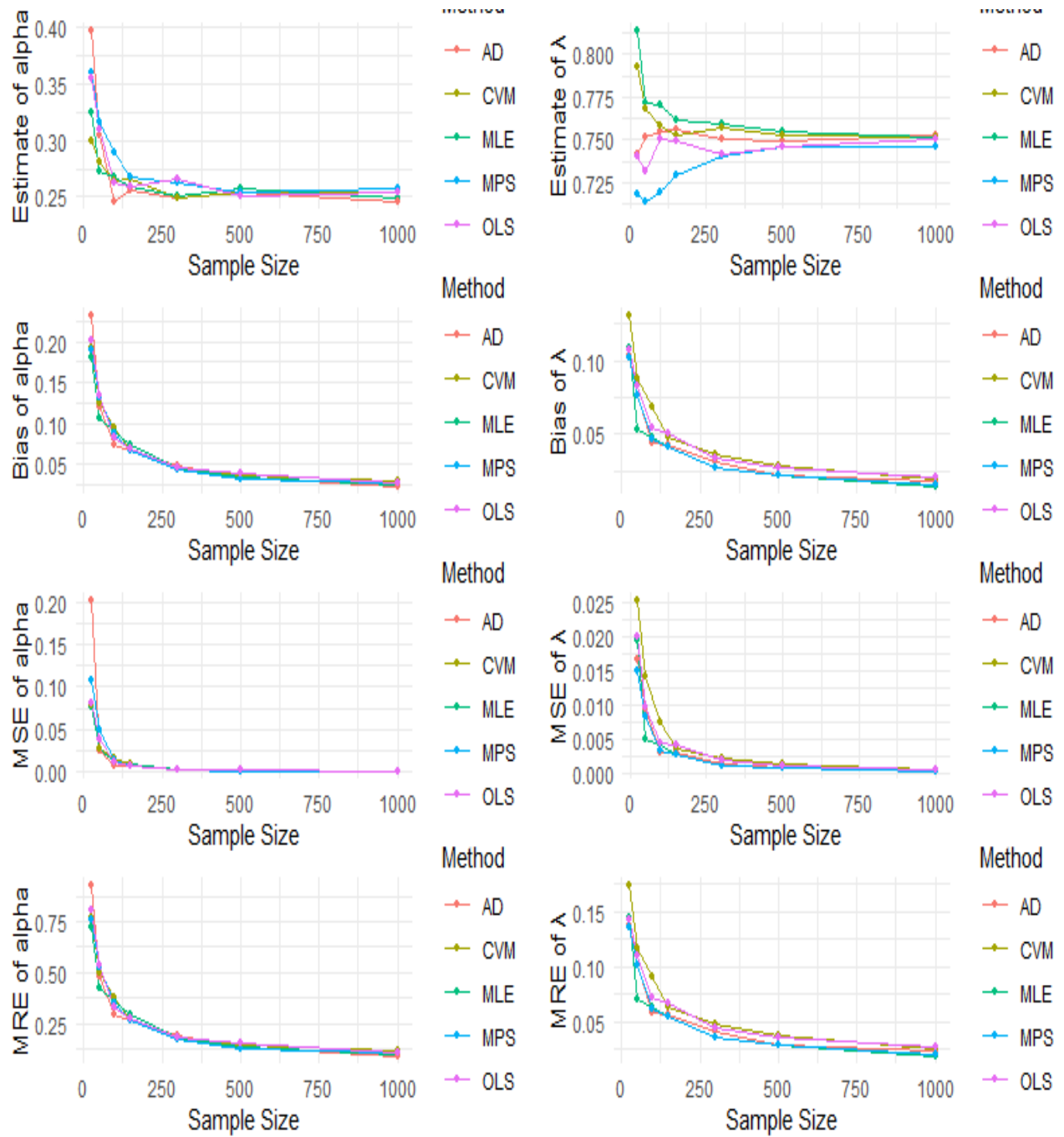


Figure 5. Graphical representation of Estimate, Bias, MSE, and MRE values presented in Table 1.

Table 2. Simulation values of Estimates, Bias, MSE, and MRE for ( $\alpha = 0.5, \lambda = 1$ ).

| Sample Size | Method | $\hat{\alpha}$ | $\hat{\lambda}$ | Bias( $\hat{\alpha}$ ) | Bias( $\hat{\lambda}$ ) | MSE( $\hat{\alpha}$ ) | MSE( $\hat{\lambda}$ ) | MRE( $\hat{\alpha}$ ) | MRE( $\hat{\lambda}$ ) |
|-------------|--------|----------------|-----------------|------------------------|-------------------------|-----------------------|------------------------|-----------------------|------------------------|
| 25          | MLE    | 0.604622       | 1.047836        | 0.335612               | 0.145728                | 0.217046              | 0.037464               | 0.671225              | 0.145728               |
| 50          | MLE    | 0.517619       | 1.010105        | 0.193513               | 0.087307                | 0.059491              | 0.012565               | 0.387026              | 0.087307               |
| 100         | MLE    | 0.498266       | 1.014357        | 0.130619               | 0.063215                | 0.026686              | 0.006716               | 0.261238              | 0.063215               |
| 150         | MLE    | 0.516519       | 1.011581        | 0.128424               | 0.048852                | 0.026613              | 0.004187               | 0.256848              | 0.048852               |
| 300         | MLE    | 0.511985       | 1.001961        | 0.089815               | 0.034152                | 0.012456              | 0.002008               | 0.179629              | 0.034152               |
| 500         | MLE    | 0.496278       | 1.008507        | 0.062265               | 0.026687                | 0.006331              | 0.001036               | 0.124529              | 0.026687               |
| 1000        | MLE    | 0.506416       | 1.004580        | 0.051366               | 0.019808                | 0.003855              | 0.000635               | 0.102731              | 0.019808               |
| 25          | AD     | 0.575676       | 1.019750        | 0.301122               | 0.128744                | 0.211167              | 0.035588               | 0.602245              | 0.128744               |
| 50          | AD     | 0.556715       | 0.997130        | 0.224822               | 0.100479                | 0.112401              | 0.015585               | 0.449643              | 0.100479               |
| 100         | AD     | 0.542661       | 1.016364        | 0.144104               | 0.065705                | 0.036198              | 0.007568               | 0.288207              | 0.065705               |
| 150         | AD     | 0.514910       | 1.001622        | 0.126531               | 0.052092                | 0.028367              | 0.004634               | 0.253062              | 0.052092               |
| 300         | AD     | 0.492253       | 0.999875        | 0.091754               | 0.041477                | 0.013160              | 0.002558               | 0.183509              | 0.041477               |
| 500         | AD     | 0.502007       | 1.003336        | 0.057953               | 0.032656                | 0.005686              | 0.001677               | 0.115905              | 0.032656               |
| 1000        | AD     | 0.499201       | 0.998304        | 0.046245               | 0.019017                | 0.003448              | 0.000543               | 0.092490              | 0.019017               |
| 25          | CVM    | 0.583454       | 1.055700        | 0.346805               | 0.159331                | 0.224253              | 0.049371               | 0.693609              | 0.159331               |
| 50          | CVM    | 0.560392       | 1.001347        | 0.244876               | 0.116635                | 0.101998              | 0.020250               | 0.489753              | 0.116635               |
| 100         | CVM    | 0.553924       | 0.992614        | 0.162703               | 0.072389                | 0.048181              | 0.007816               | 0.325405              | 0.072389               |
| 150         | CVM    | 0.515043       | 1.011700        | 0.119995               | 0.068832                | 0.023563              | 0.009268               | 0.239991              | 0.068832               |
| 300         | CVM    | 0.499455       | 1.007186        | 0.088295               | 0.045690                | 0.011263              | 0.003284               | 0.176590              | 0.045690               |
| 500         | CVM    | 0.493539       | 1.001203        | 0.073037               | 0.036136                | 0.008245              | 0.002000               | 0.146074              | 0.036136               |
| 1000        | CVM    | 0.497856       | 1.004157        | 0.048515               | 0.026809                | 0.003700              | 0.001189               | 0.097030              | 0.026809               |
| 25          | MPS    | 0.603761       | 0.925469        | 0.275039               | 0.132997                | 0.137672              | 0.027679               | 0.550078              | 0.132997               |
| 50          | MPS    | 0.565887       | 0.933412        | 0.193693               | 0.096719                | 0.068649              | 0.013239               | 0.387386              | 0.096719               |
| 100         | MPS    | 0.537141       | 0.980598        | 0.142307               | 0.061653                | 0.030917              | 0.005822               | 0.284613              | 0.061653               |
| 150         | MPS    | 0.565756       | 0.979002        | 0.135245               | 0.056873                | 0.033685              | 0.005091               | 0.270491              | 0.056873               |
| 300         | MPS    | 0.535503       | 0.980922        | 0.093439               | 0.035997                | 0.014105              | 0.001853               | 0.186879              | 0.035997               |
| 500         | MPS    | 0.524481       | 0.991853        | 0.068327               | 0.029910                | 0.007343              | 0.001412               | 0.136654              | 0.029910               |
| 1000        | MPS    | 0.494172       | 0.997925        | 0.042785               | 0.020478                | 0.003033              | 0.000690               | 0.085570              | 0.020478               |
| 25          | OLS    | 0.666928       | 1.036401        | 0.397914               | 0.182625                | 0.297665              | 0.079671               | 0.795828              | 0.182625               |
| 50          | OLS    | 0.576001       | 0.994268        | 0.212287               | 0.099645                | 0.094956              | 0.016035               | 0.424575              | 0.099645               |
| 100         | OLS    | 0.552238       | 0.981959        | 0.154626               | 0.086677                | 0.047188              | 0.010492               | 0.309252              | 0.086677               |
| 150         | OLS    | 0.508533       | 0.998313        | 0.113951               | 0.069449                | 0.021360              | 0.006893               | 0.227903              | 0.069449               |
| 300         | OLS    | 0.510027       | 0.996797        | 0.080990               | 0.049710                | 0.010379              | 0.003839               | 0.161979              | 0.049710               |
| 500         | OLS    | 0.510507       | 1.004018        | 0.066430               | 0.030823                | 0.007011              | 0.001563               | 0.132860              | 0.030823               |
| 1000        | OLS    | 0.508137       | 0.998619        | 0.053165               | 0.026633                | 0.004298              | 0.001096               | 0.106330              | 0.026633               |



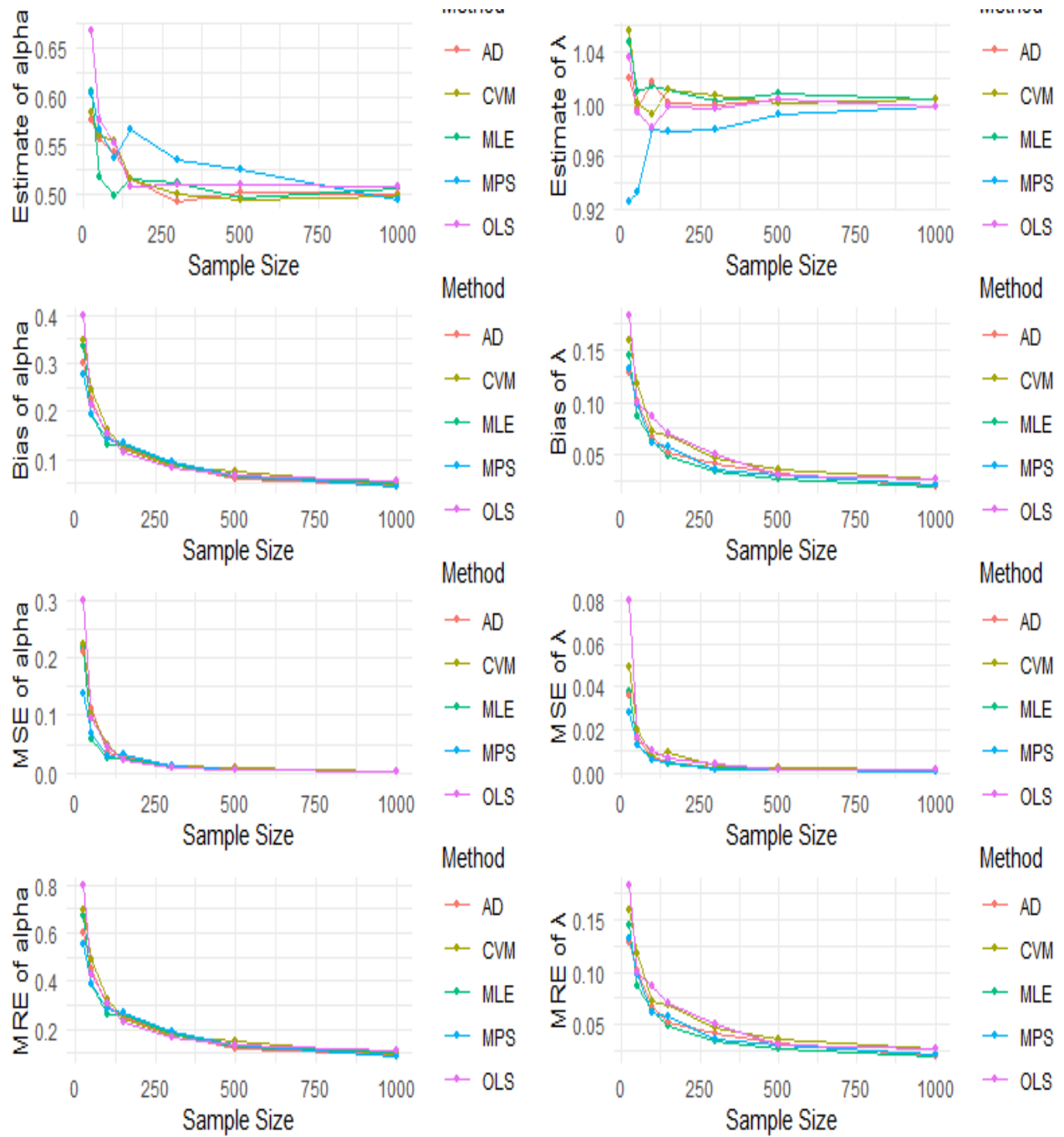


Figure 6. Graphical representation of Estimate, Bias, MSE, and MRE values presented in Table 2.

Table 3. Simulation values of Estimates, Bias, MSE, and MRE for  $(\alpha = 2, \lambda = 1)$ .

| Sample Size | Method | $\hat{\alpha}$ | $\hat{\lambda}$ | Bias( $\hat{\alpha}$ ) | Bias( $\hat{\lambda}$ ) | MSE( $\hat{\alpha}$ ) | MSE( $\hat{\lambda}$ ) | MRE( $\hat{\alpha}$ ) | MRE( $\hat{\lambda}$ ) |
|-------------|--------|----------------|-----------------|------------------------|-------------------------|-----------------------|------------------------|-----------------------|------------------------|
| 25          | MLE    | 3.212831       | 1.067780        | 2.008607               | 0.125458                | 11.573667             | 0.032344               | 1.004304              | 0.125458               |
| 50          | MLE    | 2.233042       | 1.028175        | 0.887122               | 0.076538                | 1.346299              | 0.011634               | 0.443561              | 0.076538               |
| 100         | MLE    | 2.182920       | 1.005188        | 0.623708               | 0.053182                | 0.860550              | 0.004656               | 0.311854              | 0.053182               |
| 150         | MLE    | 1.971027       | 0.996391        | 0.395466               | 0.041949                | 0.247083              | 0.003001               | 0.197733              | 0.041949               |
| 300         | MLE    | 2.122692       | 1.011020        | 0.425895               | 0.033407                | 0.319862              | 0.001742               | 0.212948              | 0.033407               |
| 500         | MLE    | 2.020594       | 1.005905        | 0.255106               | 0.029985                | 0.105357              | 0.001272               | 0.127553              | 0.029985               |
| 1000        | MLE    | 2.012578       | 0.998449        | 0.162673               | 0.016597                | 0.047159              | 0.000440               | 0.081337              | 0.016597               |
| 25          | AD     | 2.933367       | 1.007198        | 1.506997               | 0.120514                | 11.956806             | 0.021521               | 0.753499              | 0.120514               |
| 50          | AD     | 2.165274       | 1.006941        | 0.812413               | 0.083725                | 1.359413              | 0.012374               | 0.406207              | 0.083725               |
| 100         | AD     | 2.112530       | 0.998841        | 0.531703               | 0.060039                | 0.529811              | 0.005870               | 0.265851              | 0.060039               |
| 150         | AD     | 2.208226       | 1.009680        | 0.553967               | 0.049818                | 0.554768              | 0.004523               | 0.276983              | 0.049818               |
| 300         | AD     | 1.987243       | 0.994139        | 0.306564               | 0.041227                | 0.142356              | 0.002721               | 0.153282              | 0.041227               |
| 500         | AD     | 2.049418       | 1.000130        | 0.232564               | 0.026023                | 0.090476              | 0.001150               | 0.116282              | 0.026023               |
| 1000        | AD     | 2.009585       | 0.997505        | 0.177858               | 0.019207                | 0.052310              | 0.000597               | 0.088929              | 0.019207               |
| 25          | CVM    | 2.562685       | 1.023676        | 1.344952               | 0.158900                | 6.203513              | 0.042634               | 0.672476              | 0.158900               |
| 50          | CVM    | 2.198450       | 1.015783        | 0.808844               | 0.112450                | 1.225484              | 0.023045               | 0.404422              | 0.112450               |
| 100         | CVM    | 2.157844       | 0.998602        | 0.522876               | 0.072332                | 0.452549              | 0.008609               | 0.261438              | 0.072332               |
| 150         | CVM    | 1.982215       | 1.003727        | 0.459847               | 0.060209                | 0.395603              | 0.005596               | 0.229924              | 0.060209               |
| 300         | CVM    | 2.083594       | 1.002607        | 0.372878               | 0.042888                | 0.217785              | 0.002876               | 0.186439              | 0.042888               |
| 500         | CVM    | 2.089927       | 0.996862        | 0.271897               | 0.030191                | 0.138053              | 0.001304               | 0.135949              | 0.030191               |
| 1000        | CVM    | 2.019047       | 1.003084        | 0.185343               | 0.023690                | 0.050599              | 0.000928               | 0.092671              | 0.023690               |
| 25          | MPS    | 2.322445       | 0.906181        | 1.122302               | 0.136755                | 2.811999              | 0.026985               | 0.561151              | 0.136755               |
| 50          | MPS    | 2.385805       | 0.961383        | 0.773570               | 0.085553                | 1.292548              | 0.010449               | 0.386785              | 0.085553               |
| 100         | MPS    | 2.189917       | 0.974577        | 0.597207               | 0.059745                | 0.569064              | 0.005025               | 0.298603              | 0.059745               |
| 150         | MPS    | 2.199184       | 0.988174        | 0.455814               | 0.053204                | 0.524846              | 0.004061               | 0.227907              | 0.053204               |
| 300         | MPS    | 2.102561       | 0.989501        | 0.290804               | 0.035801                | 0.156821              | 0.001922               | 0.145402              | 0.035801               |
| 500         | MPS    | 2.034230       | 0.987667        | 0.229667               | 0.025709                | 0.094513              | 0.001027               | 0.114833              | 0.025709               |
| 1000        | MPS    | 2.025788       | 0.992832        | 0.163091               | 0.020662                | 0.061937              | 0.000654               | 0.081545              | 0.020662               |
| 25          | OLS    | 2.794893       | 1.010620        | 1.481708               | 0.173504                | 6.340959              | 0.051214               | 0.740854              | 0.173504               |
| 50          | OLS    | 2.141161       | 1.020272        | 0.745891               | 0.106810                | 1.115792              | 0.017786               | 0.372945              | 0.106810               |
| 100         | OLS    | 2.186301       | 0.991772        | 0.686903               | 0.069867                | 0.867224              | 0.008199               | 0.343451              | 0.069867               |
| 150         | OLS    | 2.089332       | 0.997897        | 0.444889               | 0.061191                | 0.315059              | 0.005769               | 0.222444              | 0.061191               |
| 300         | OLS    | 2.030200       | 0.997201        | 0.303155               | 0.042940                | 0.140567              | 0.002951               | 0.151578              | 0.042940               |
| 500         | OLS    | 2.027001       | 0.996773        | 0.267153               | 0.033483                | 0.110639              | 0.001629               | 0.133577              | 0.033483               |
| 1000        | OLS    | 2.003389       | 1.005798        | 0.157795               | 0.026513                | 0.042861              | 0.001047               | 0.078898              | 0.026513               |

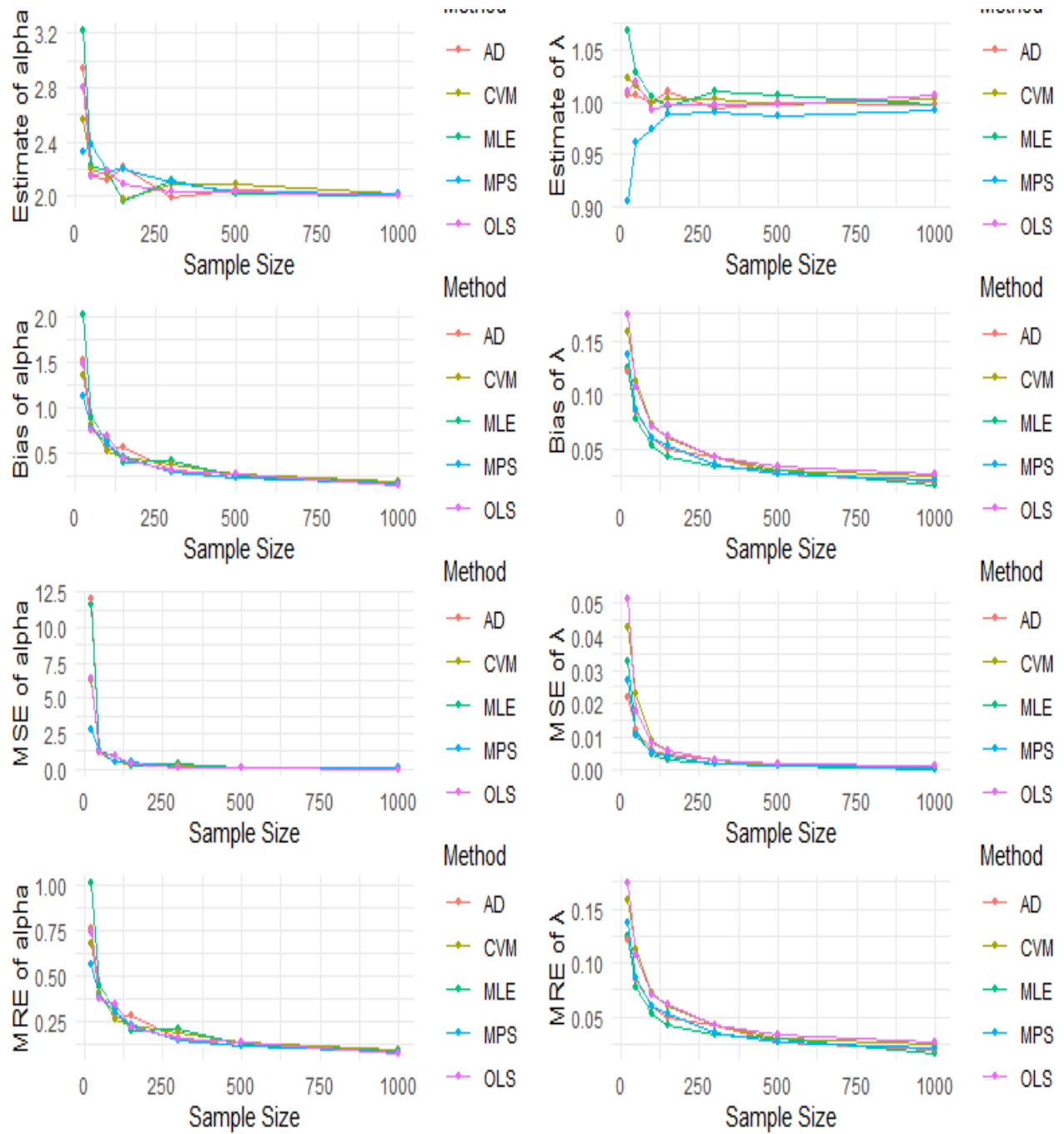


Figure 7. Graphical representation of Estimate, Bias, MSE, and MRE values presented in Table 3.

Table 4. Simulation values of Estimates, Bias, MSE, and MRE for  $(\alpha = 1, \lambda = 1)$ .

| Sample Size | Method | $\hat{\alpha}$ | $\hat{\lambda}$ | Bias( $\hat{\alpha}$ ) | Bias( $\hat{\lambda}$ ) | MSE( $\hat{\alpha}$ ) | MSE( $\hat{\lambda}$ ) | MRE( $\hat{\alpha}$ ) | MRE( $\hat{\lambda}$ ) |
|-------------|--------|----------------|-----------------|------------------------|-------------------------|-----------------------|------------------------|-----------------------|------------------------|
| 25          | MLE    | 1.000000       | 1.043379        | 0.000000               | 0.138504                | 0.000000              | 0.034957               | 0.000000              | 0.138504               |
| 50          | MLE    | 1.000000       | 1.013742        | 0.000000               | 0.084444                | 0.000000              | 0.011718               | 0.000000              | 0.084444               |
| 100         | MLE    | 1.000000       | 1.001318        | 0.000000               | 0.055014                | 0.000000              | 0.005235               | 0.000000              | 0.055014               |
| 150         | MLE    | 1.000000       | 1.014566        | 0.000000               | 0.044767                | 0.000000              | 0.003222               | 0.000000              | 0.044767               |
| 300         | MLE    | 1.000000       | 1.001807        | 0.000000               | 0.035574                | 0.000000              | 0.001927               | 0.000000              | 0.035574               |
| 500         | MLE    | 1.000000       | 0.998352        | 0.000000               | 0.024632                | 0.000000              | 0.000948               | 0.000000              | 0.024632               |
| 1000        | MLE    | 1.000000       | 1.000111        | 0.000000               | 0.016885                | 0.000000              | 0.000487               | 0.000000              | 0.016885               |
| 25          | AD     | 1.000000       | 0.950257        | 0.000000               | 0.134100                | 0.000000              | 0.028746               | 0.000000              | 0.134100               |
| 50          | AD     | 1.000000       | 0.982530        | 0.000000               | 0.100758                | 0.000000              | 0.015885               | 0.000000              | 0.100758               |
| 100         | AD     | 1.000000       | 0.992657        | 0.000000               | 0.063703                | 0.000000              | 0.006305               | 0.000000              | 0.063703               |
| 150         | AD     | 1.000000       | 0.986089        | 0.000000               | 0.056962                | 0.000000              | 0.005152               | 0.000000              | 0.056962               |
| 300         | AD     | 1.000000       | 0.991485        | 0.000000               | 0.039224                | 0.000000              | 0.002617               | 0.000000              | 0.039224               |
| 500         | AD     | 1.000000       | 1.005577        | 0.000000               | 0.034094                | 0.000000              | 0.001850               | 0.000000              | 0.034094               |
| 1000        | AD     | 1.000000       | 0.998423        | 0.000000               | 0.021410                | 0.000000              | 0.000773               | 0.000000              | 0.021410               |
| 25          | CVM    | 1.000000       | 1.009650        | 0.000000               | 0.205481                | 0.000000              | 0.079776               | 0.000000              | 0.205481               |
| 50          | CVM    | 1.000000       | 1.016141        | 0.000000               | 0.131566                | 0.000000              | 0.030086               | 0.000000              | 0.131566               |
| 100         | CVM    | 1.000000       | 0.993484        | 0.000000               | 0.094587                | 0.000000              | 0.013029               | 0.000000              | 0.094587               |
| 150         | CVM    | 1.000000       | 0.992549        | 0.000000               | 0.076261                | 0.000000              | 0.008857               | 0.000000              | 0.076261               |
| 300         | CVM    | 1.000000       | 1.007258        | 0.000000               | 0.053902                | 0.000000              | 0.004705               | 0.000000              | 0.053902               |
| 500         | CVM    | 1.000000       | 0.996156        | 0.000000               | 0.040162                | 0.000000              | 0.002374               | 0.000000              | 0.040162               |
| 1000        | CVM    | 1.000000       | 0.994240        | 0.000000               | 0.027664                | 0.000000              | 0.001222               | 0.000000              | 0.027664               |
| 25          | MPS    | 1.000000       | 0.922500        | 0.000000               | 0.127447                | 0.000000              | 0.025582               | 0.000000              | 0.127447               |
| 50          | MPS    | 1.000000       | 0.941602        | 0.000000               | 0.096777                | 0.000000              | 0.013453               | 0.000000              | 0.096777               |
| 100         | MPS    | 1.000000       | 0.973487        | 0.000000               | 0.062208                | 0.000000              | 0.006019               | 0.000000              | 0.062208               |
| 150         | MPS    | 1.000000       | 0.975185        | 0.000000               | 0.054526                | 0.000000              | 0.004502               | 0.000000              | 0.054526               |
| 300         | MPS    | 1.000000       | 0.988498        | 0.000000               | 0.035935                | 0.000000              | 0.001886               | 0.000000              | 0.035935               |
| 500         | MPS    | 1.000000       | 0.990280        | 0.000000               | 0.028205                | 0.000000              | 0.001246               | 0.000000              | 0.028205               |
| 1000        | MPS    | 1.000000       | 0.991401        | 0.000000               | 0.019585                | 0.000000              | 0.000559               | 0.000000              | 0.019585               |
| 25          | OLS    | 1.000000       | 0.921417        | 0.000000               | 0.197258                | 0.000000              | 0.066185               | 0.000000              | 0.197258               |
| 50          | OLS    | 1.000000       | 0.958158        | 0.000000               | 0.115767                | 0.000000              | 0.020936               | 0.000000              | 0.115767               |
| 100         | OLS    | 1.000000       | 0.978956        | 0.000000               | 0.087494                | 0.000000              | 0.012557               | 0.000000              | 0.087494               |
| 150         | OLS    | 1.000000       | 0.983878        | 0.000000               | 0.069138                | 0.000000              | 0.007375               | 0.000000              | 0.069138               |
| 300         | OLS    | 1.000000       | 0.993597        | 0.000000               | 0.050315                | 0.000000              | 0.003943               | 0.000000              | 0.050315               |
| 500         | OLS    | 1.000000       | 0.998652        | 0.000000               | 0.035044                | 0.000000              | 0.001961               | 0.000000              | 0.035044               |
| 1000        | OLS    | 1.000000       | 0.996512        | 0.000000               | 0.030609                | 0.000000              | 0.001492               | 0.000000              | 0.030609               |

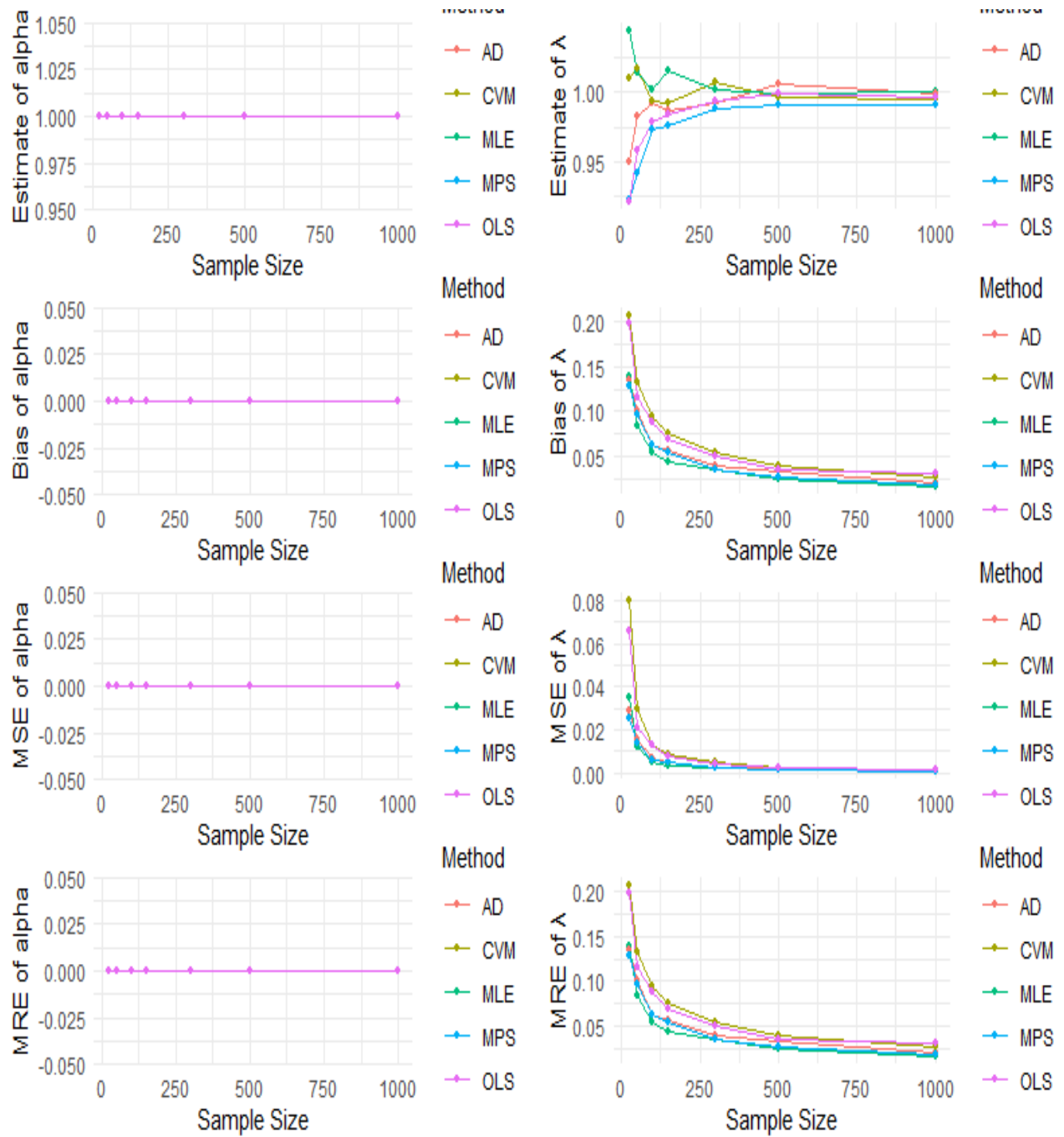


Figure 8. Graphical representation of Estimate, Bias, MSE, and MRE values presented in Table 4.

## 6. Model Comparison in Fitting to Real Data Sets

Two real datasets were analyzed to illustrate the applicability of the proposed distribution. The first dataset comprises the remission times of 128 bladder cancer patients (Aldeni et al., 2017)[23], which naturally aligns with the survival/lifetime framework. The second dataset included 24 determinations of copper concentration (in ppm) in wholemeal flour (Analytical Methods Committee, 1989)[26]. Although this dataset is not a lifetime dataset, it was selected to test the model's flexibility in fitting positive and skewed data, highlighting its potential utility beyond traditional survival analysis. This section compares the APOPW distribution to other comparable lifetime distributions, such as the Power XLindley [27], Gamma Lindley [24], Gamma, Quasi Lindley [20], New Quasi Lindley [15], NTPQED [29], Two parameter Lindley2 [28]. The maximum likelihood estimates were obtained numerically by minimizing the negative log-likelihood function using the BFGS quasi-Newton method implemented in the `optim()` function in R. Convergence was declared when the relative change in both the parameter estimates and the objective function was below  $10^{-8}$ , with a maximum of 1000 iterations. Initial guesses for  $(\alpha, \beta)$  were set close to the true parameter values in the simulation study, while for real data they were chosen based on simple moment-based heuristics. To avoid convergence to local optima, several perturbed starting values were also tested, and the solution yielding the largest likelihood was retained. And to compare several distributions, we consider criteria like AIC (Akaike Information Criterion), BIC (Bayesian Information Criterion), -2LL (-2Log-Likelihood), and CAIC (Consistent Akaike Information Criterion), HQIC (Hannan-Quinn information criterion) for the data set. The better distribution corresponds to smaller AIC, BIC, -2LL, CAIC and HQIC values.

The first data set consists of the remission time of 128 bladder cancer patients. The data were taken from Aldeni et al. (2017) [23].

**The dataset 1 are:** 0.080, 0.200, 0.400, 0.500, 0.510, 0.810, 0.900, 1.050, 1.190, 1.260, 1.350, 1.400, 1.460, 1.760, 2.020, 2.020, 2.070, 2.090, 2.230, 2.260, 2.460, 2.540, 2.620, 2.640, 2.690, 2.690, 2.750, 2.830, 2.870, 3.020, 3.250, 3.310, 3.360, 3.360, 3.480, 3.520, 3.570, 3.640, 3.700, 3.820, 3.880, 4.180, 4.230, 4.260, 4.330, 4.340, 4.400, 4.500, 4.510, 4.870, 4.980, 5.060, 5.090, 5.170, 5.320, 5.320, 5.340, 5.410, 5.410, 5.490, 5.620, 5.710, 5.850, 6.250, 6.540, 6.760, 6.930, 6.940, 6.970, 7.090, 7.260, 7.280, 7.320, 7.390, 7.590, 7.620, 7.630, 7.660, 7.870, 7.930, 8.260, 8.370, 8.530, 8.650, 8.660, 9.020, 9.220, 9.470, 9.740, 10.06, 10.34, 10.66, 10.75, 11.25, 11.64, 11.79, 11.98, 12.02, 12.03, 12.07, 12.63, 13.11, 13.29, 13.80, 14.24, 14.76, 14.77, 14.83, 15.96, 16.62, 17.12, 17.14, 17.36, 18.10, 19.13, 20.28, 21.73, 22.69, 23.63, 25.74, 25.82, 26.31, 32.15, 34.26, 36.66, 43.01, 46.12, 79.05

Table 5. MLEs of the parameters estimated for real dataset 1

| Distribution           | $\hat{\alpha}$  | $\hat{\lambda}$  | $\hat{\theta}$ | $\hat{b}$  |
|------------------------|-----------------|------------------|----------------|------------|
| Power XLindley         | 1.388593        |                  | 0.2612941      |            |
| Gamma Lindley          |                 |                  | 0.1069747      | 0.09678821 |
| Gamma                  |                 | 0.1251788        | 1.172319       |            |
| Quasi Lindley          |                 | 0.3160336        | 0.04183527     |            |
| New Quasi Lindley      |                 | 0.1140924        | 0.0005250499   |            |
| NTPQED                 |                 |                  | 0.1885692      | 88.3213    |
| Two parameter Lindley2 | 0.1077796       |                  | 0.000843786    |            |
| Two parameter Lindley1 | 0.1069879       |                  | 4722.193       |            |
| Weibull                |                 | 1.047849         | 9.561373       |            |
| APOPWD                 | <b>434.8434</b> | <b>0.4671386</b> |                |            |

The second dataset is a numeric vector of 24 determinations of copper in wholemeal flour, expressed in parts per million. Data were taken from the Analytical Methods Committee (1989) [26].

Table 6. Analytical measures of fit criteria for survival time data of cancer (dataset 1)

| Distribution           | AIC             | BIC             | -2LL            | CAIC            | HQIC           |
|------------------------|-----------------|-----------------|-----------------|-----------------|----------------|
| Power XLindley         | 1127.514        | 1133.218        | 1123.514        | 1127.610        | 1129.831       |
| Gamma Lindley          | 832.6839        | 838.3879        | 828.6839        | 832.7799        | 835.0015       |
| Gamma                  | 830.7356        | 836.4396        | 826.7356        | 830.8316        | 833.0531       |
| Quasi Lindley          | 1196.427        | 1202.131        | 1192.427        | 1196.523        | 1198.745       |
| New Quasi Lindley      | 832.8294        | 838.5334        | 828.8294        | 832.9254        | 835.147        |
| NTPQED                 | 841.4313        | 847.1353        | 837.4313        | 841.5273        | 843.7489       |
| Two parameter Lindley2 | 832.686         | 838.3901        | 828.686         | 832.782         | 835.0036       |
| Two parameter Lindley1 | 832.6839        | 838.388         | 828.6839        | 832.7799        | 835.0015       |
| Weibull                | 832.1738        | 837.8778        | 828.1738        | 832.2698        | 834.4913       |
| APOPWD                 | <b>830.2344</b> | <b>835.9385</b> | <b>826.2344</b> | <b>830.3304</b> | <b>832.552</b> |

**The dataset 2 are:** 2.90, 3.10, 3.40, 3.40, 3.70, 3.70, 2.80, 2.50, 2.40, 2.40, 2.70, 2.20, 5.28, 3.37, 3.03, 3.03, 28.95, 3.77, 3.40, 2.20, 3.50, 3.60, 3.70, 3.70

Table 7. MLEs of the parameters estimated for real dataset 2

| Distribution           | $\hat{\alpha}$  | $\hat{\lambda}$  | $\hat{\theta}$ | $\hat{b}$  |
|------------------------|-----------------|------------------|----------------|------------|
| Power XLindley         | 1.484577        |                  | 0.33913        |            |
| Gamma Lindley          |                 |                  | 0.4643355      | 35.07353   |
| Gamma                  |                 | 0.574331         | 2.458373       |            |
| Quasi Lindley          |                 | 0.7888356        | 0.00041516     |            |
| New Quasi Lindley      |                 | 0.4639805        | 29.20064       |            |
| NTPQED                 |                 |                  | 0.6523102      | 0.00062837 |
| Two parameter Lindley2 | 0.4634209       |                  | 39.34863       |            |
| Two parameter Lindley1 | 0.4762804       |                  | 0.4750378      |            |
| Weibull                |                 | 1.230793         | 4.673114       |            |
| <b>APOPWD</b>          | <b>126.2734</b> | <b>0.6975994</b> |                |            |

Table 8. Analytical measures of fit criteria for survival time data of copper in wholemeal flour (dataset 2)

| Distribution           | AIC             | BIC             | -2LL            | CAIC            | HQIC            |
|------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Power XLindley         | 177.3466        | 179.7027        | 173.3466        | 177.918         | 177.9716        |
| Gamma Lindley          | 113.8102        | 116.1663        | 109.8102        | 114.3816        | 114.4353        |
| Gamma                  | 113.1218        | 115.4779        | 109.1218        | 113.6932        | 113.7469        |
| Quasi Lindley          | 140.8624        | 143.2185        | 136.8624        | 141.4338        | 141.4875        |
| New Quasi Lindley      | 113.7834        | 116.1395        | 109.7834        | 114.3549        | 114.4085        |
| NTPQED                 | 114.4569        | 116.8130        | 110.4569        | 115.0284        | 115.0820        |
| Two parameter Lindley2 | 113.8517        | 116.2078        | 109.8517        | 114.4231        | 114.4767        |
| Two parameter Lindley1 | 116.8540        | 119.2101        | 112.8540        | 117.4255        | 117.4791        |
| Weibull                | 119.4160        | 121.7721        | 115.4160        | 119.9874        | 120.0411        |
| <b>APOPWD</b>          | <b>112.1528</b> | <b>114.5089</b> | <b>108.1528</b> | <b>112.7242</b> | <b>112.7779</b> |

According to Tables 6,8, we can observe that APOPW distribution provide smallest AIC, BIC, -2LL, CAIC, HQIC values as compared to Power XLindley, gamma Lindley, gamma, quasi Lindley, new quasi Lindley, NTPQED, two-parameter L2, two parameter L1, and Weibull distributions, and hence best fits the data among all the models considered.

## 7. Conclusion

In this paper, we proposed a new lifetime distribution, the Alpha Power One-Parameter Weibull (APOPW) distribution with two shape parameters, which extends the one-parameter Weibull distribution. The proposed distribution exhibits desirable properties such as unimodality, light tails, and flexible hazard rate shapes. These features make it particularly suitable for modeling lifetime and reliability data. We explored its key mathematical and statistical properties, including the cumulative distribution function, probability density function, moments (including mean, variance), moment-generating function, quantile function, mean deviation, Rényi and Shannon entropy, stress-strength reliability, mean deviations, and extreme order statistics.

Multiple parameter estimation methods were considered, and a comprehensive simulation study was conducted to evaluate estimation accuracy of five different methods for estimating the unknown parameters. The comprehensive simulation results, based on metrics such as average absolute bias (BAIS), mean squared error (MSE), and mean absolute relative error (MRE), indicate that the maximum likelihood estimation (MLE) method is the most efficient and reliable approach.

Furthermore, applications to two real datasets confirmed the superiority of the APOPW over several well-known distributions, such as the Power XLindley, Gamma Lindley, Gamma, Quasi Lindley, New Quasi Lindley, TPQED, Two parameter Lindley2, Two parameter Lindley1, and Weibull. Based on model selection criteria such as AIC (Akaike Information Criterion), BIC (Bayesian Information Criterion), -2LL (-2Log-Likelihood), and CAIC (Consistent Akaike Information Criterion), HQIC (Hannan-quinn information criterion), the APOPW distribution consistently provided the best fit to the data.

Overall, the Alpha Power One-Parameter Weibull (APOPW) distribution offers significant flexibility and modeling power under uncertainty, making it a valuable addition to the family of lifetime distributions, and the second dataset (copper in flour) is not a lifetime dataset, it was included to demonstrate the flexibility of the proposed model in handling different types of positive and skewed data, highlighting its potential utility beyond traditional survival analysis.

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